



Arsenic Removal from Water using Iron Oxide Ceramic Membranes

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Problem



- Norman pays Oklahoma City \$3.10/1000 gallons for drinking water
- Previously from Lake Thunderbird and Norman wells (Well flow rates of 1500 m³/day)
- Arsenic (As) concentrations range from 1 to 42 parts per billion (ppb)
- Lung, skin, urinary, bladder, and kidney cancers caused by As poisoning

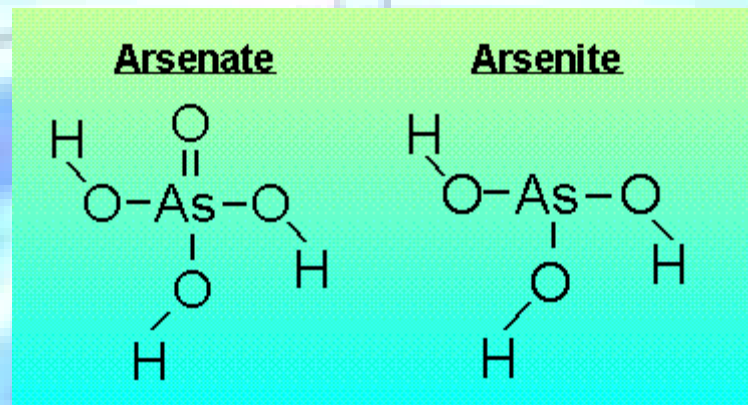


Challenge

- Reduce concentrations to World Health Organization (WHO) standards of 10 ppb
- Evaluate iron oxide ceramic membranes to remove this arsenic
- Design treatment system using membranes

Background

- Arsenate and arsenite are common forms of arsenic found in water



- Research at UT-El Paso found that these two forms adsorbed to iron oxide coated stones



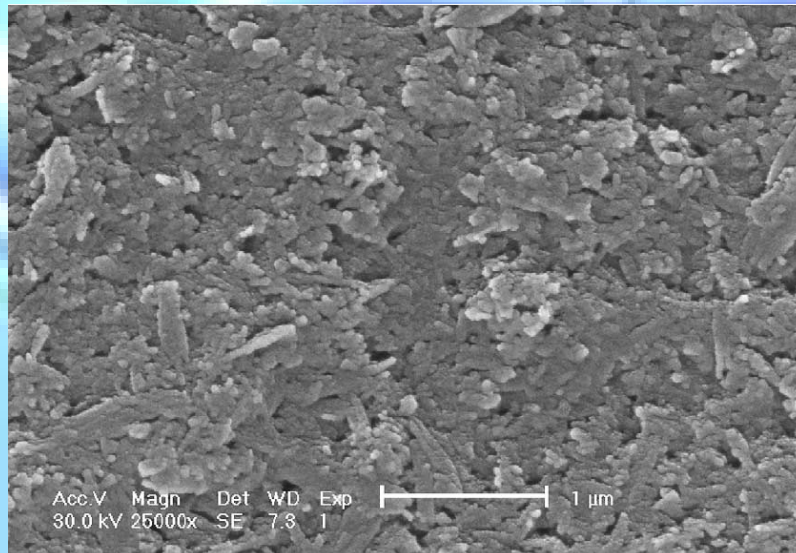
Background

- Under Dr. Maria Fidalgo de Cortalezzi, current research is being performed on iron oxide membranes at El Instituto Tecnológico de Buenos Aires

Saturation Limit:	0.00011	kg As/kg Fe ₂ O ₃
Porosity:	0.4	
Fe ₂ O ₃ on pilot membrane:	0.002	kg
Membrane thickness, l_m :	50	μm
Pore diameter:	24	nm
Flux:	9.02×10^{-5}	$\text{m}^3/\text{m}^2\text{s}$
BET Surface Area:	120	m^2/g

Background

- Pressure difference across membrane drives contaminated water across membrane
- Arsenic adsorbs to iron oxide membrane



SEM image of top the top surface of an iron oxide membrane

From Cortalezzi, et al.



Challenge

- Must treat 8 contaminated wells with an iron oxide membrane system
 - Membrane Design Limitations:
 - Size (Brittleness, transporting...)
 - Porosity
 - Thickness
 - Saturation time



Design Proposals

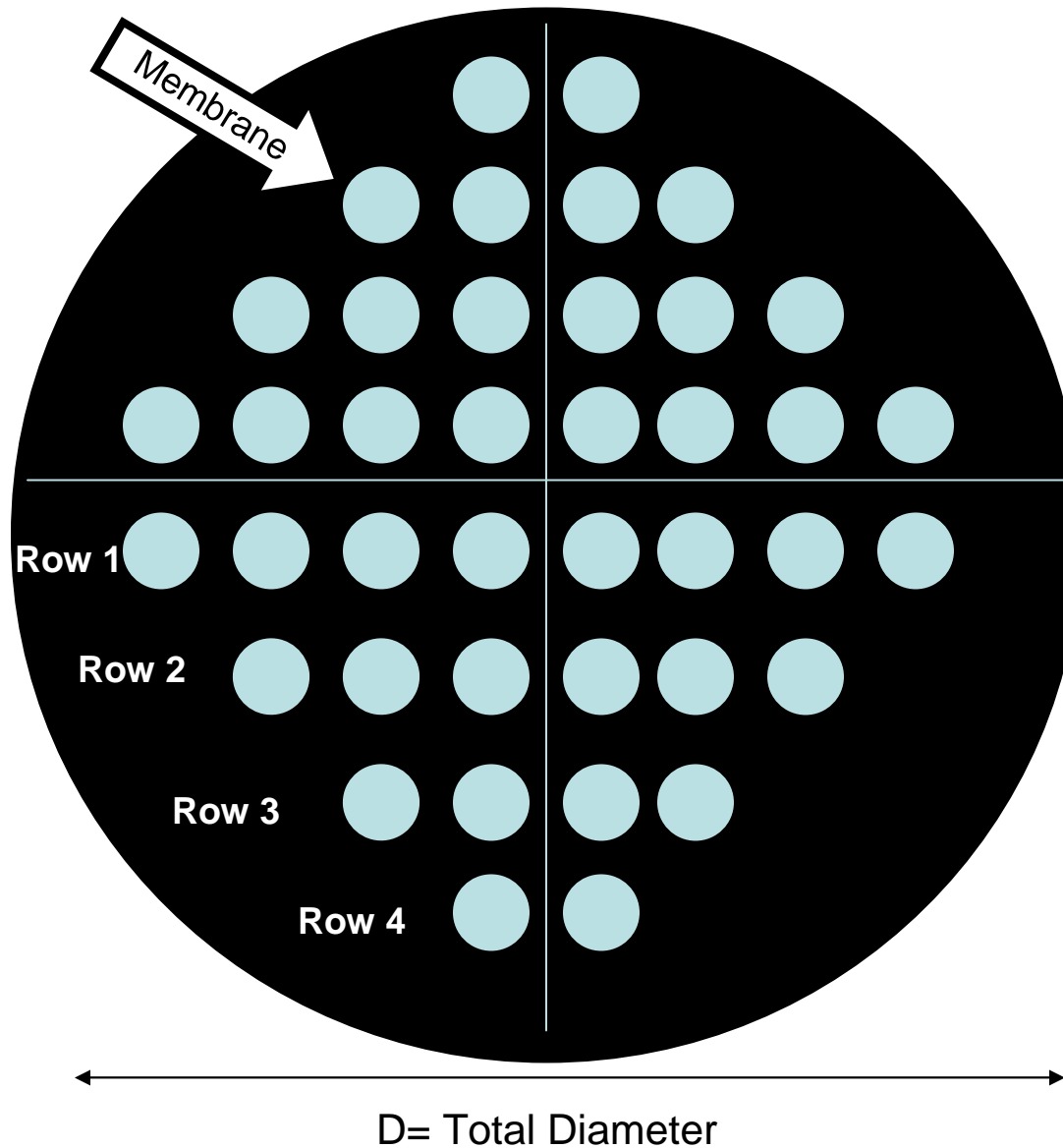
Municipal Treatment System

1. Large membrane to place inside 33" pipe
 - Too brittle
 - Cannot transport
 - High production costs
- ✓ 2. Small membranes to make up 33" pipe
 - Sturdy
 - Low production costs

At-Home Treatment System

3. Membrane size of faucet
 - High consumer costs

Scale Up



D = Total diameter of support (inches)

$D_{\text{membrane}} + \text{Clearance} = 3$ inches

n = number of membranes

Looking at 1 quadrant of support:

Row 1: $n = D / (2 * (D_{\text{membrane}} + \text{Clearance}))$

Row 2: $n = (D/6) - 1$

Row 3: $n = (D/6) - 2$

Row 4: $n = (D/6) - 3 = (D/6) - ((D/6) - 1)$

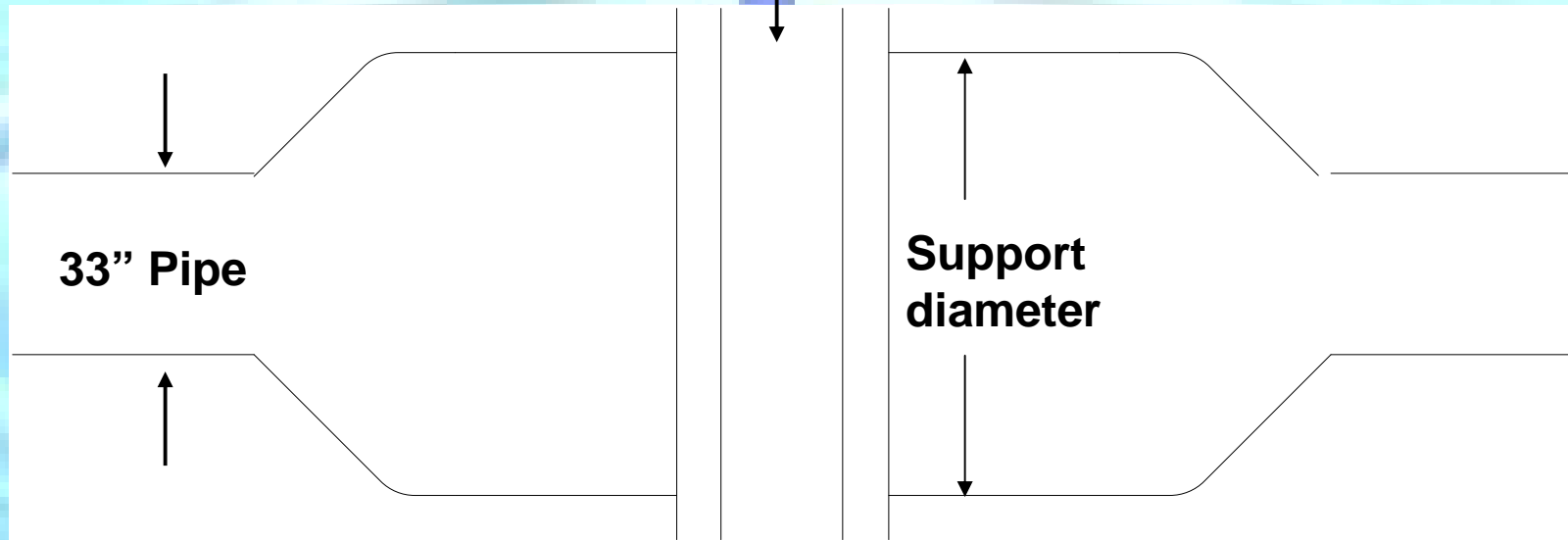
Continue for any diameter and multiply by four for number of quadrants:

$$n = 4 * \sum_{x=0}^{\frac{D}{6}-1} \left(\frac{D}{6} - x \right)$$

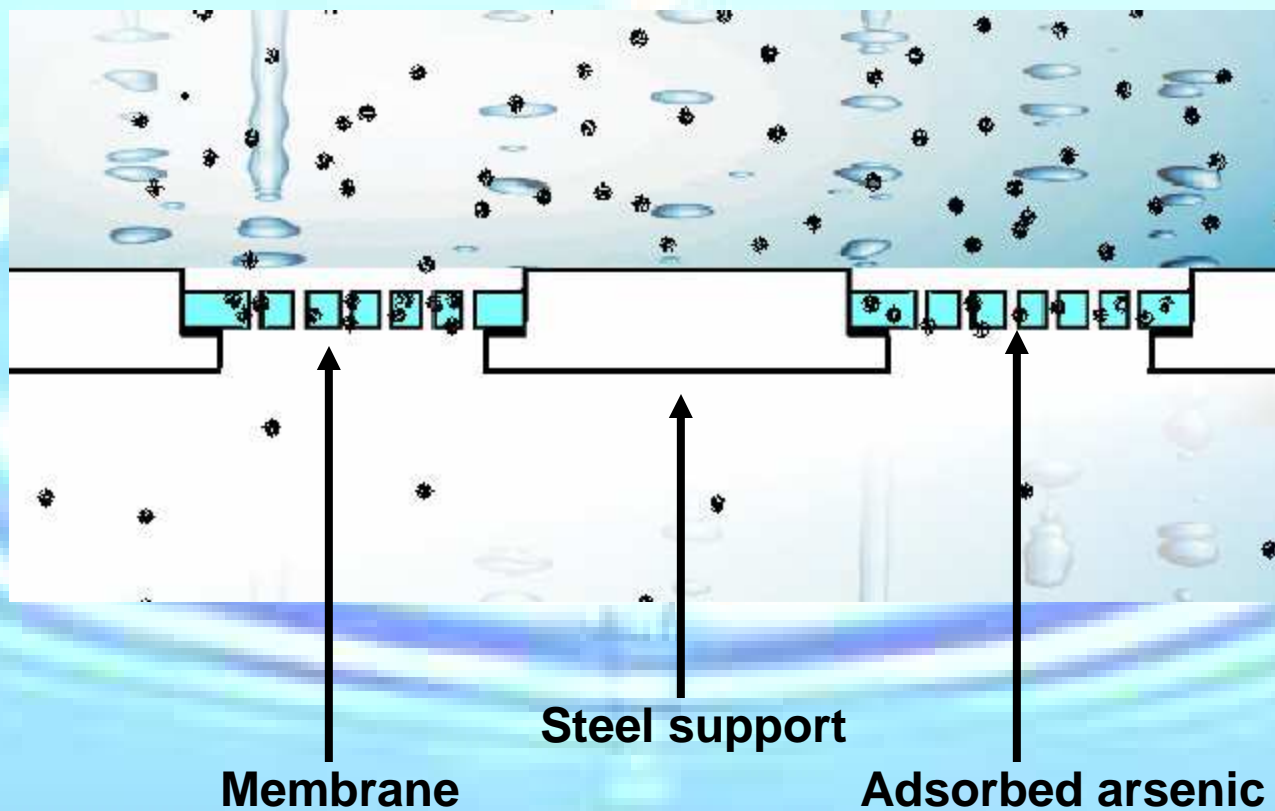


Chosen Design

Insert membranes in support



Chosen Design



Pressure Drop Across Membrane

Modified Ergun Equation, derived from Darcy's Law for dead-end filtration, laminar flow of spherical particles (arsenic) in solution (water) into a porous membrane

$$\rho Q_{well} = \frac{\rho \varepsilon^3 (P_{in} - P_{out})}{(150 / 36)(1 - \varepsilon)^2 a_v^2 \mu l_M}$$

Bernoulli Equation for work of the pump

$$\frac{\Delta P}{\rho} + \frac{\Delta(v^2)}{2} + g\Delta z = \frac{W}{\rho Q_{well}} \Rightarrow W = Q_{well} \Delta P$$

Required Pump Work

$$W = Q_{well} \Delta P = \frac{Q_{well}^2 \left((150/36)(1-\varepsilon)^2 a_v^2 \mu l_M \right)}{\varepsilon^3}$$

Where Q_{well} = volumetric flow rate of water

ε = porosity

D_{pore} = pore diameter

n = number of pores

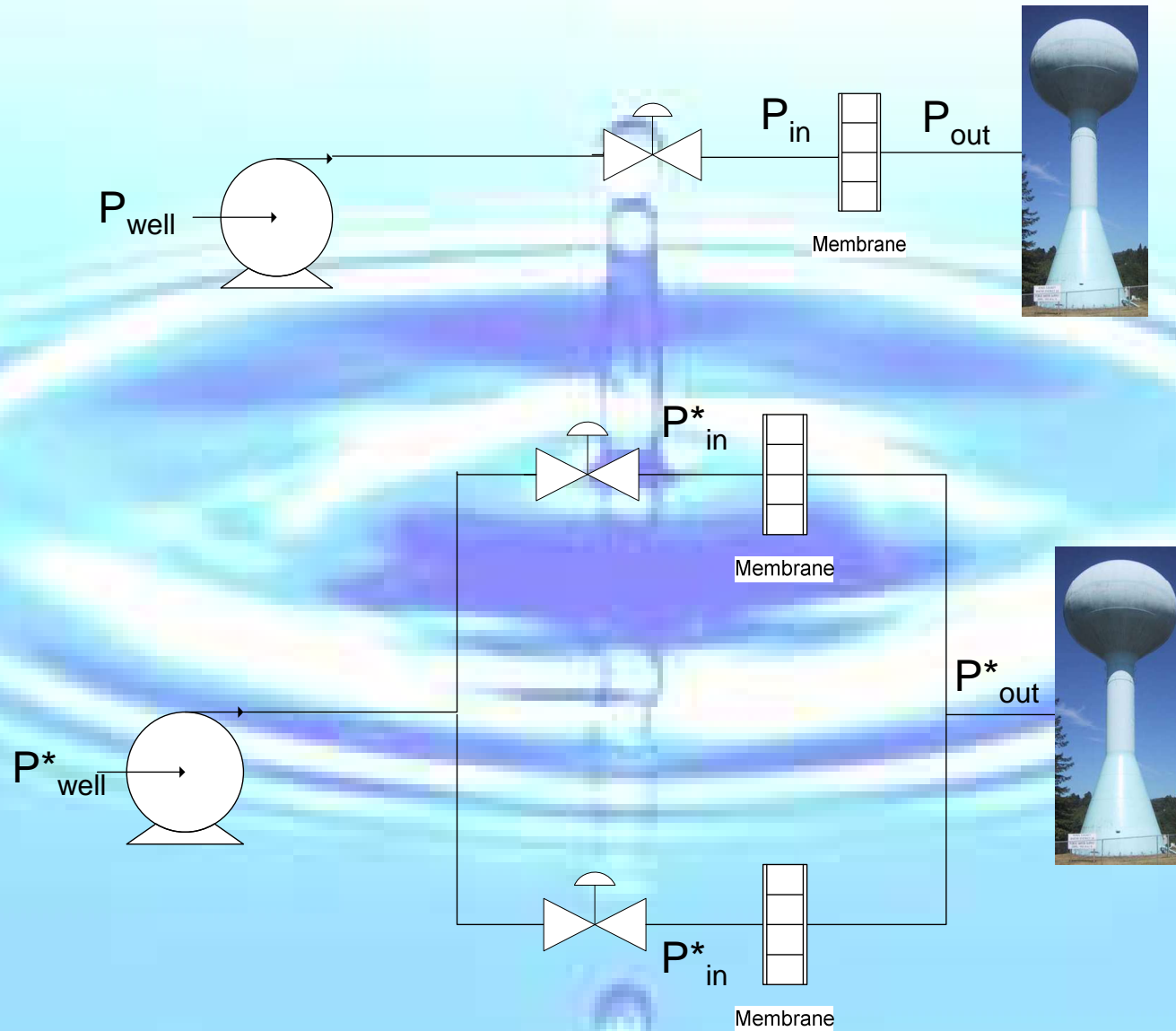
a_v = specific surface area of membrane

μ = fluid viscosity

l_M = membrane thickness

$150/36 = 2 \cdot \text{tortuosity}$

Municipal System



Pump Work Comparison

$$\rho Q_{\text{well}} = \frac{\rho \varepsilon^3 (P_{\text{in}} - P_{\text{out}})}{(150/36)(1 - \varepsilon)^2 a_v^2 \mu l_M} \Rightarrow P_{\text{in}} = Q_{\text{well}} \alpha + P_{\text{out}}$$

Full Flow

$$P_{\text{in}} = Q_{\text{well}} \alpha + P_{\text{out}}$$

$$\Delta P = P_{\text{in}} - P_{\text{out}} = Q_{\text{well}} \alpha$$

$$\begin{aligned} W_{\text{pump}} &= Q_{\text{well}} (P_{\text{in}} - P_{\text{well}}) \\ &= Q_{\text{well}} (Q_{\text{well}} \alpha + P_{\text{out}} - P_{\text{well}}) \end{aligned}$$

$$P_{\text{out}} = P_{\text{well}}$$

$$W_{\text{pump}} = Q_{\text{well}} (Q_{\text{well}} \alpha)$$

$$\boxed{W_{\text{pump}} = Q_{\text{well}}^2 \alpha}$$

Split Flow

$$P_{\text{in}}^* = (Q_{\text{well}}/2) \alpha + P_{\text{out}}^*$$

$$\Delta P^* = P_{\text{in}}^* - P_{\text{out}}^* = (Q_{\text{well}}/2) \alpha$$

$$\begin{aligned} W_{\text{pump}}^* &= Q_{\text{well}} (P_{\text{in}}^* - P_{\text{well}}^*) \\ &= Q_{\text{well}} [(Q_{\text{well}}/2) \alpha + P_{\text{out}}^* - P_{\text{well}}^*] \end{aligned}$$

$$P_{\text{out}}^* = P_{\text{well}}^*$$

$$W_{\text{pump}}^* = Q_{\text{well}} [(Q_{\text{well}}/2) \alpha]$$

$$\boxed{W_{\text{pump}}^* = Q_{\text{well}}^2 \alpha / 2}$$

Work to Remove Water from Well and Pump to Holding Tanks

- Each well supplies water at 1500 m³/day
- Assume this same flow rate to holding tanks approximately 10 miles away
- Bernoulli Equation with frictional losses through 33" pipe

$$\frac{\Delta P}{\rho} + \frac{\Delta(v^2)}{2} + g\Delta z + \sum F = W$$

Turbulent Flow

$$f = \frac{0.079}{\text{Re}^{0.25}}$$

$$F = \frac{2fV^2L}{D}$$

Time of Saturation

$$t_{\text{saturation}} = \frac{(0.00011 \text{ kgAs} / \text{kgFe}_2\text{O}_3) * x_{\text{kg, ironoxide}}}{\text{As}_{\text{flow}}}$$

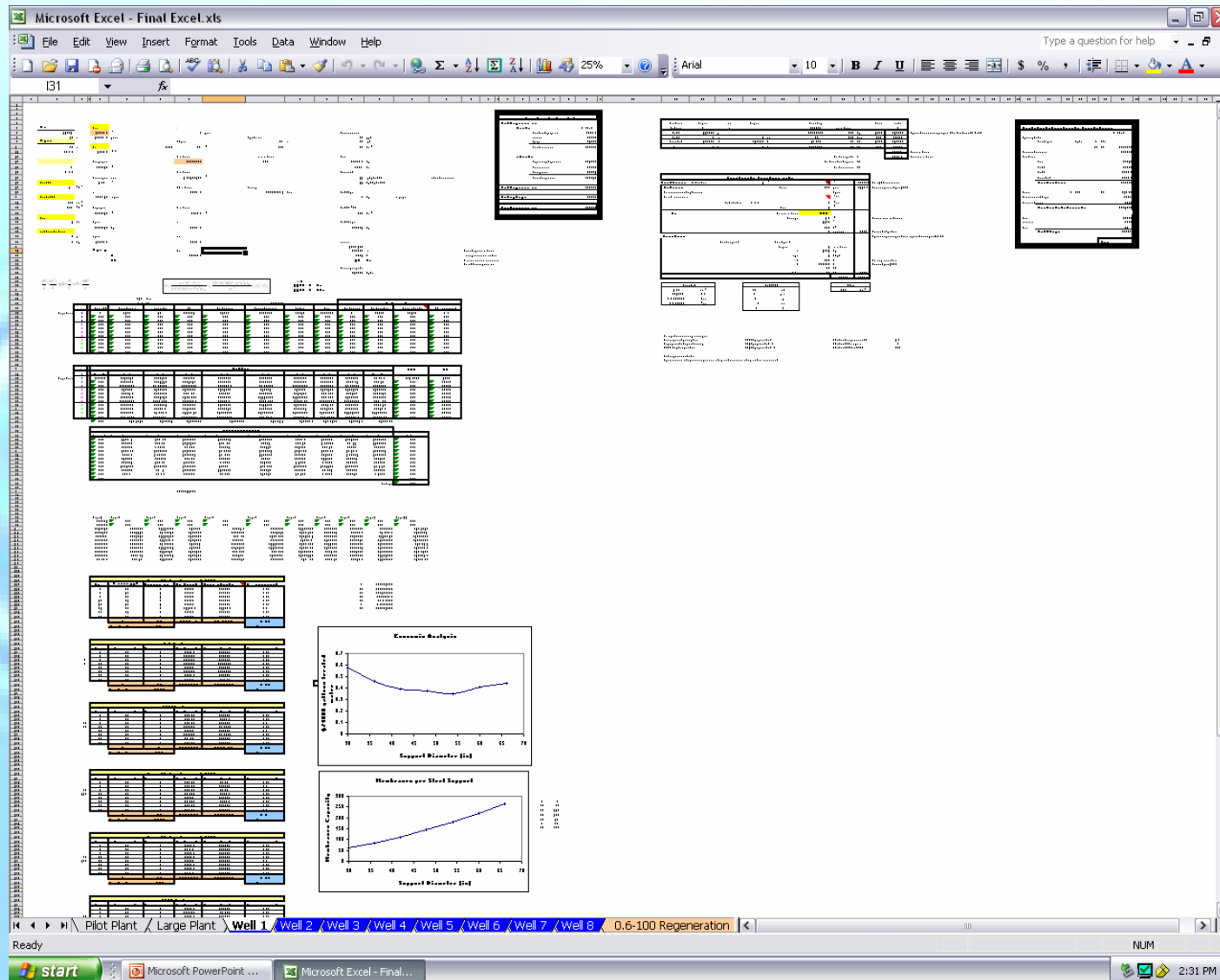
Regeneration with Basic Wash

$$\text{1st flush: } t_{\text{saturation}} = t_{\text{saturation}} + 0.5t_{\text{saturation}}$$

$$\text{2nd flush: } t_{\text{saturation}} = t_{\text{saturation}} + 0.5t_{\text{saturation}} + 0.25t_{\text{saturation}}$$

$$\text{3rd flush: } t_{\text{saturation}} = t_{\text{saturation}} + 0.5t_{\text{saturation}} + 0.25t_{\text{saturation}} + 0.125t_{\text{saturation}}$$

Scale Up



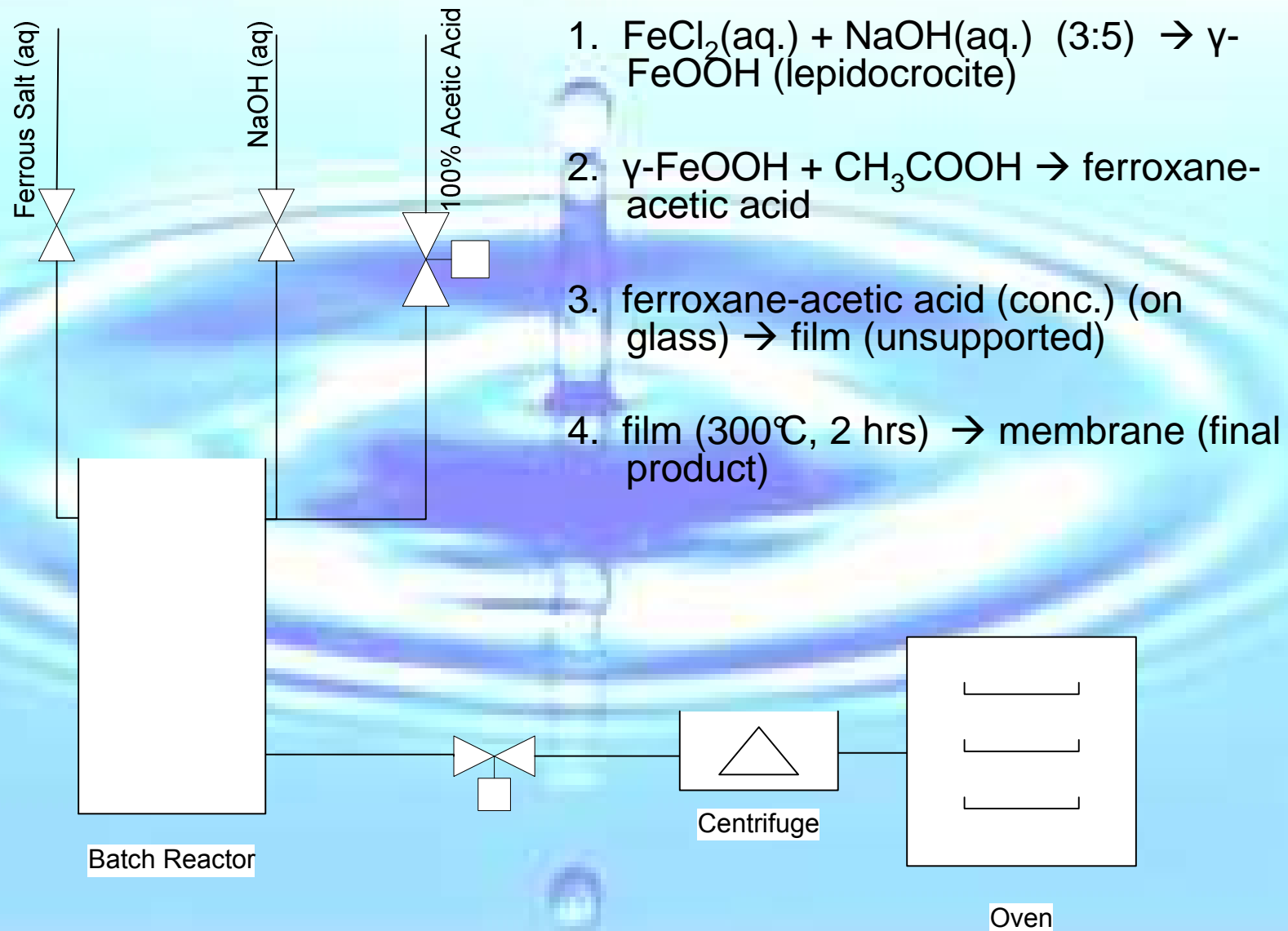
Pump Work and Saturation Time

- Chose to vary following parameters:
 - Support diameter
 - Arsenic concentration
 - Flow rate from well
- With more research, in the future, can vary:
 - Pore diameter
 - Membrane thickness
 - Membrane diameter
 - Porosity

Pump Work and Saturation Time

	D_{as}		Q_{well}		ε		As_{concentration}
2	1.15E-10 (m)		0.0174 (m ³ /s)		0.4 porosity		32 (ppb)
3	0.12 (nm)		1.45E+08 gal/year		SA_{pores}		0.032 (mg/L)
4	D_{pore}		Flux		240 (m ²)		0.000032 (kg/m ³)
5	24 (nm)		0.016 (m ³ /m ² s)		R_{membrane}		As_{flow}
6	2.40E-08 (m)		A_{cs single pore}		0.035786997		5.556E-07 (kg/s)
7	l_m		4.52E-16 (m ²)		A_{membrane}		17.52 (kg/yr)
8	50 (μm)		A_{cs every pore} flow/flux		1.062195148 (m ²)		Saturation Limit
9	5.00E-05 (m)		1.06E+00 (m ²)		SA_{membrane}		0.11 (mg As/g Fe ₂ O ₃)
10			n		8.85E+03		0.00011 (kg As/kg Fe ₂ O ₃)
11	Denisty H ₂ O		2.35E+15 (# of pores)		V_{membrane}		Fe₂O₃/m² SA
12	1000 (kg/m ³)		Q_{single pore}		5.31E-05 (m ³)		1.24 (kg/m ²)
13	Denisty Fe ₂ O ₃		7.394E-18 (m ³ /s)				Fe₂O₃ needed
14	5.26 (g/cm ³)		N_{pore}		Ergun Parameters		78738.1 (kg)
15	5260 (kg/m ³)		7.394E-15 (kg/s)		a		
16	Viscosity		V_{pore}		4.52E+06 (m ²)		
17	0.001 (Pa-s)		1.634E-02 (m/s)		a_v		
18	Fe ₂ O ₃ on Membrane				7.53E+06 (m ²)		
19	2 (g)				Re		
20	0.002 (kg)				3.923E-04		
21							
22	Support diameter		ΔP		W_{pump}		t_{saturation}
23	66.0 (in)		1154063.95 (Pa)		20035.82 (W)		15590149 (s)
24	1.68 (m)		1154.06 (kPa)		20.04 (kW)		259836 (min)
25							4331 (hr)
26	# of membranes within support						180 (days)
27	264						
28							

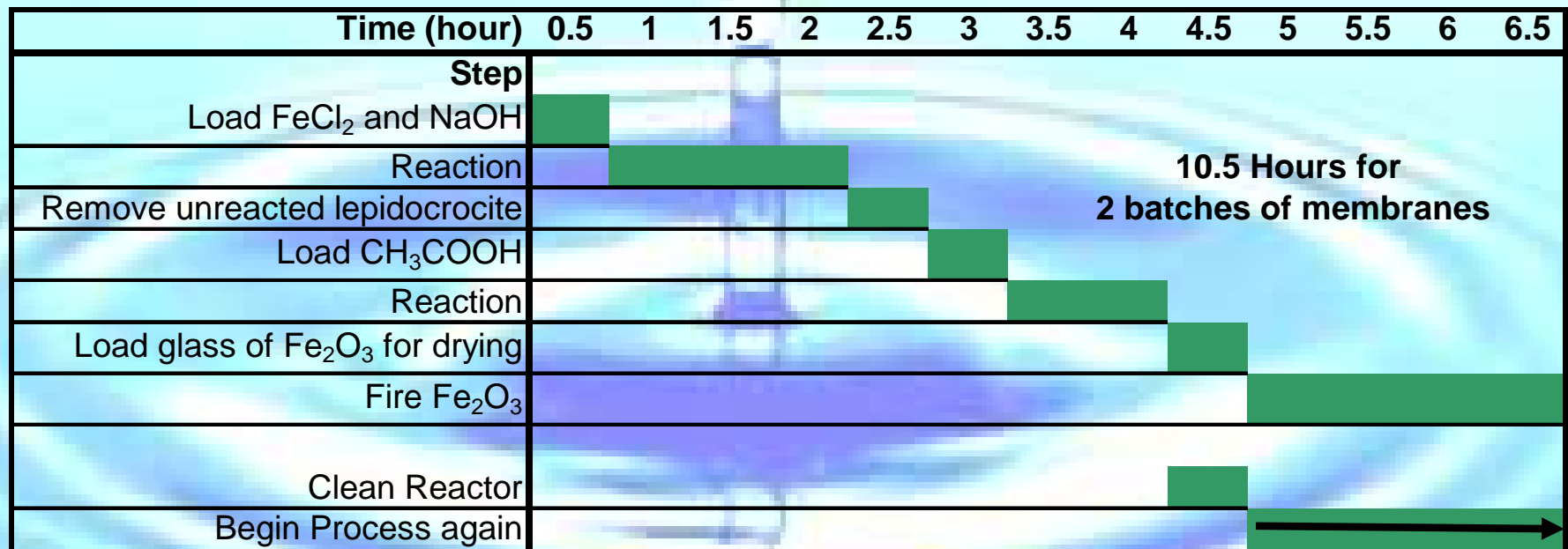
Production of Membrane



Membrane Synthesis

- Equipment required
 - 1 carbon steel batch reactor (size based on capacity)
 - Centrifuge to remove unreacted lepidocrocite
 - Glass for membrane drying
 - Batch Oven

Production Time



Plant Capacity

Chose steel support of D=30 inches

$D_{\text{membrane}} + \text{Clearance} = 3$ inches

$$n = 4 * \sum_{x=0}^{\frac{D}{6}-1} \left(\frac{D}{6} - x \right)$$

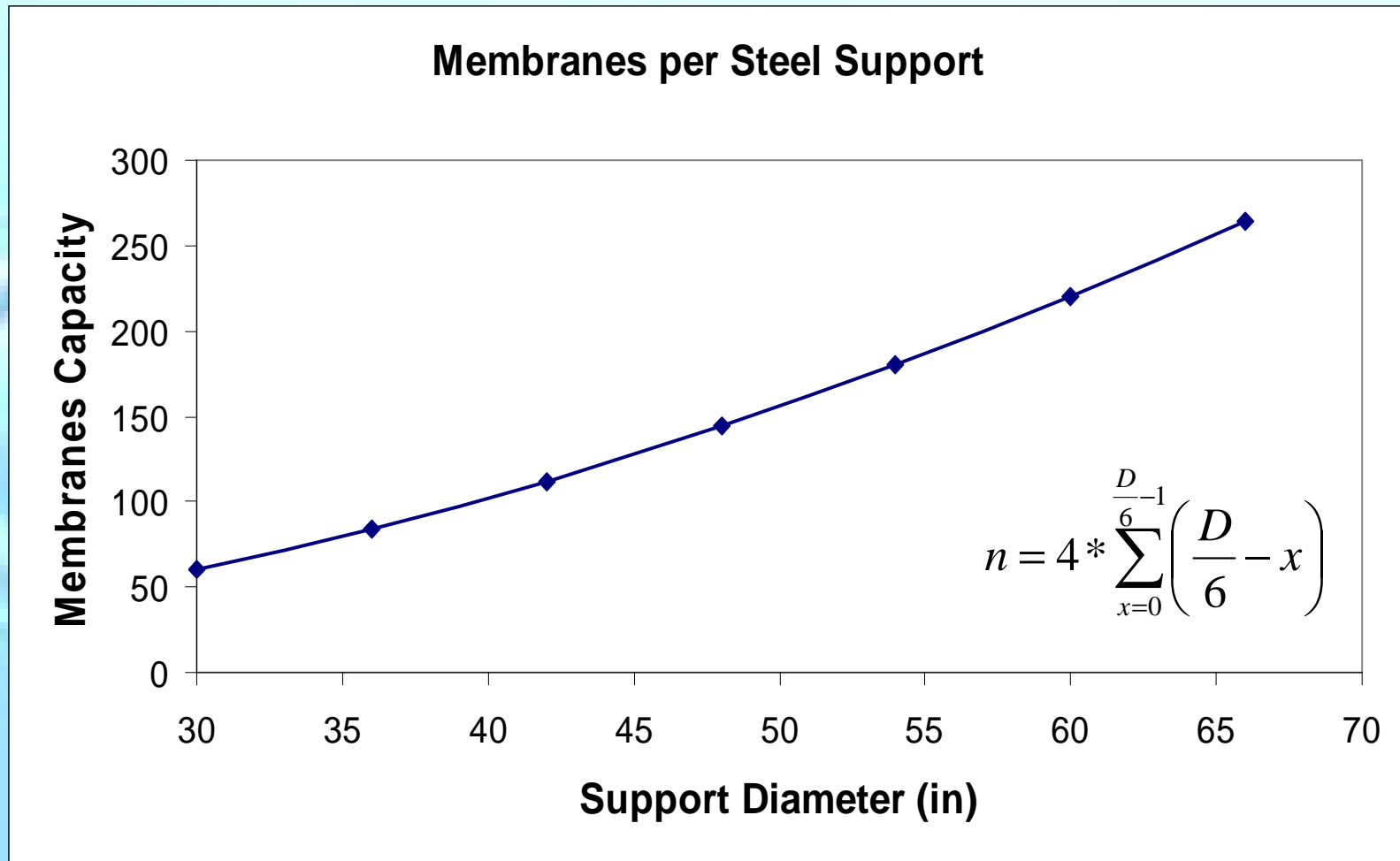
$$n = 4 * \sum_{x=0}^{\frac{30}{6}-1=4} \left(\frac{30}{6} - x \right) = 60 \text{ membranes}$$

Norman Water Wells

Well #	Asconc (ppb)	Replacements/yr
4	29	12
6	16	4
7	24	8
15	41	18
18	13	2
31	42	18
32	31	12
36	12	2
Total:		76
Total Membranes:		3800

Plant Capacity: Produce 3800+10 membranes per year

Membranes per Steel Support



Raw Materials

Raw Materials							
Produces							
FeCl ₂	1.19286 g	--	--	59643	0.000374 \$/g	22.3	\$22.31
NaOH	0.01 mol	4E-07 ton	0.02	165	\$/ton	3.3	\$3.30
Acetic Acid	1.35688 mL	0.003138 lb	157	0.25	\$/lb	19.6	\$19.61
Water	0.1 L	0.1 kg	5000	0.00055	\$/kg	2.8	\$2.75
Batch of membranes							\$47.97

Equipment



Batch Oven Specifications

- Reach temperature of 400°C
- Hold two glass shelves with area of total membranes on support
- Electrically heated
- Blower to circulate air
- Ventilation to remove evaporating water

Equipment Costs

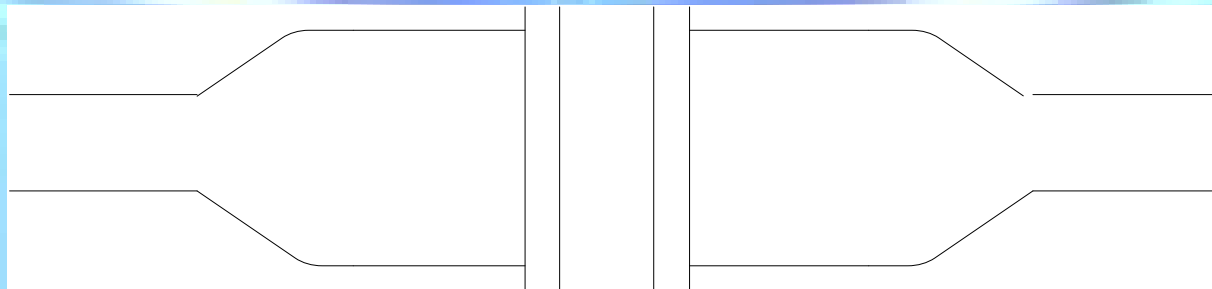
Membrane Equipment Costs					
Batch Reactor	Carbon Steel	0.000 m ³ /s	0.05 m ³	\$1,200	
Centrifuge *Remove unreacted lepidocrocite by centrifuging for 30 minutes				\$5,500	
Glass	Total diameter of membranes:		0.91 m	\$223	
	Area of glass:		0.66 m ²		
			7.07 ft ²		
			15.75 \$/ft ²		
			2 levels of glass		
Furnace & Blower					
	Inside dimensions	Recirculated Air Volume	Output	\$7,000	
	WxLxH	1600 ft ³ /min	500000 Btu/hr		
	3'x3'x4'	45.3 m ³ /min	147 kW		
				TOTAL:	\$13,923

Fixed Capital Investment

Fixed Capital Investment	
Direct Costs	2007 Costs (\$)
<i>Purchased equipment</i>	\$13,811
<i>Installation</i>	\$2,762
<i>Piping</i>	\$552
<i>Total direct plant cost</i>	\$17,126
Indirect Costs	
<i>Engineering & supervision</i>	\$11,049
<i>Legal expenses</i>	\$3,729
<i>Contingency</i>	\$2,072
<i>Total indirect plant cost</i>	\$16,850
Fixed Capital Investment	\$33,976

Working Capital

Working Capital	\$47,425
<i>Steel Support (36 inches)</i>	\$1,325
<i>Additional 33" Pipe (\$225/meter)</i>	\$2,250
<i>Increased Piping at Well (\$300/meter)</i>	\$2,400
<i>Pipe Preparation</i>	\$1,250
<i>Flanged Valve</i>	\$5,000
<i>Raw Materials</i>	\$7,100
<i>Labor & Installation</i>	\$13,000
<i>Engineer</i>	\$7,500
<i>Installation Equipment Rental</i>	\$4,500
<i>Taxes</i>	\$3,100





Production Costs

Total Product Cost - Large Scale Membrane Production			
			2007 Costs (\$)
Operating Labor			
Plant Capacity	30 (hr/day)		
	21 (\$/hr)		\$195,458
Operating Supervision			\$78,183
Raw Materials			
Water			\$828
NaOH			\$993
FeCl ₂			\$6,714
Acetic Acid			\$5,903
Total Raw Materials			\$14,439
Electricity	0.05 (\$/kW)	90925 (kW)	\$4,092
Maintenance & Repairs			\$2,039
Operating Supplies			\$306
Total Variable Production Costs			\$294,515
Royalties (membrane patent)			\$2,166
Taxes			\$4,077
Insurance			\$3,398
Rent			\$30,000
Fixed Charges			\$39,640
Total:			\$334,156



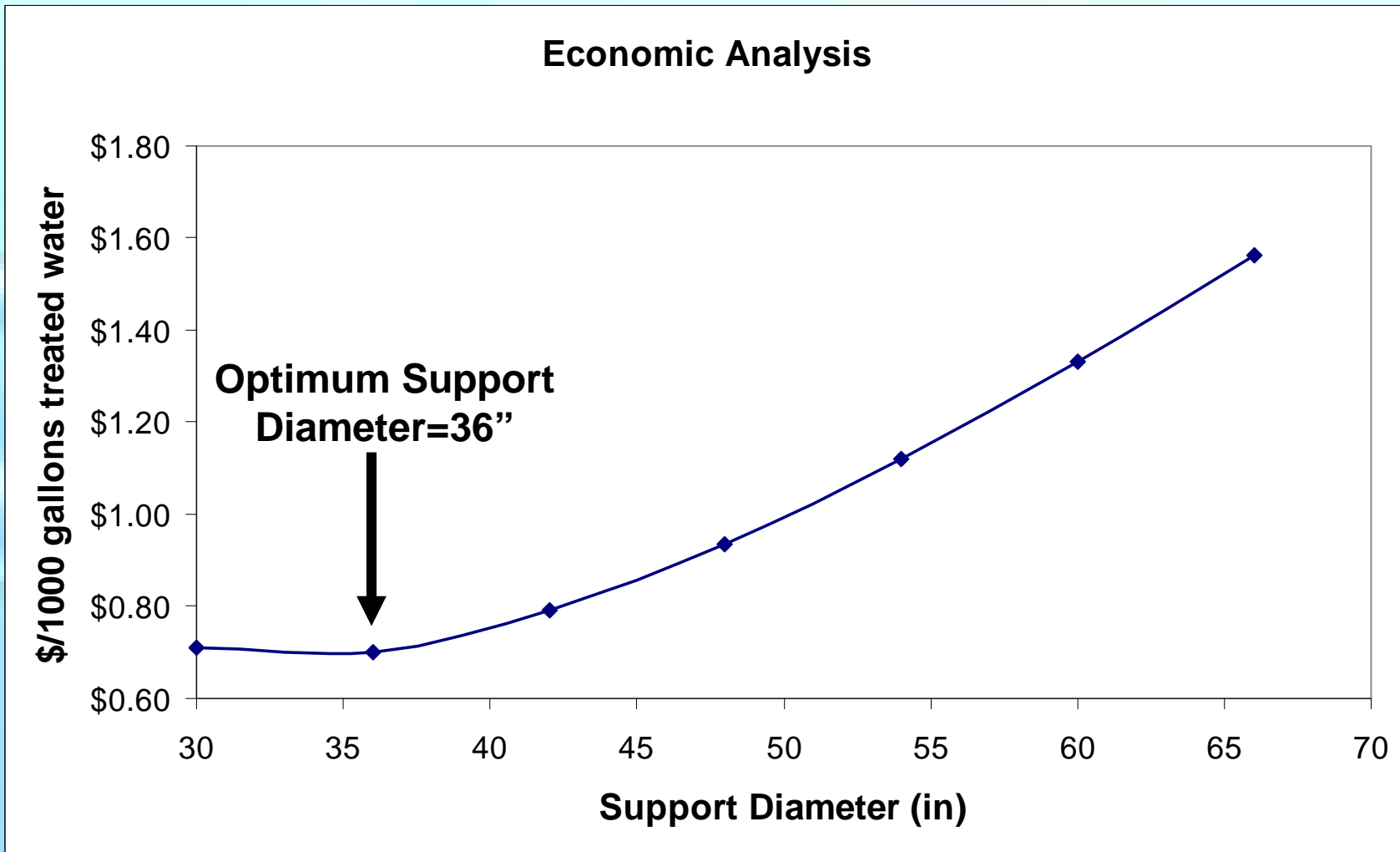
Vary Support Diameters

36"-84 Membranes/support						
Well #	Asconc (ppb)	Replacements/yr	Membrane \$/yr	Elec \$/yr from ground + to holding tanks	Consumer Total Cost/yr	\$/1000 gallons treated
4	29	8	\$72,839	\$33,029	\$105,868	\$0.73
6	16	4	\$36,420	\$33,029	\$69,449	\$0.48
7	24	6	\$54,629	\$33,029	\$87,659	\$0.61
15	41	14	\$127,468	\$33,029	\$160,498	\$1.11
18	13	2	\$18,210	\$33,029	\$51,239	\$0.35
31	42	14	\$127,468	\$33,029	\$160,498	\$1.11
32	31	10	\$91,049	\$33,029	\$124,078	\$0.86
36	12	2	\$18,210	\$33,029	\$51,239	\$0.35
Total:		60	\$546,293	\$264,235	\$810,528	\$0.70
Total Membranes:		3000				Average

42"-112 Membranes/support						
Well #	Asconc (ppb)	Replacements/yr	Membrane \$/yr	Elec \$/yr from ground + to holding tanks	Consumer Total Cost/yr	\$/1000 gallons treated
4	29	6	\$94,721	\$23,548	\$118,269	\$0.82
6	16	2	\$31,574	\$23,548	\$55,122	\$0.38
7	24	6	\$94,721	\$23,548	\$118,269	\$0.82
15	41	10	\$157,868	\$23,548	\$181,416	\$1.25
18	13	2	\$31,574	\$23,548	\$55,122	\$0.38
31	42	10	\$157,868	\$23,548	\$181,416	\$1.25
32	31	8	\$126,294	\$23,548	\$149,843	\$1.04
36	12	2	\$31,574	\$23,548	\$55,122	\$0.38
Total:		46	\$726,191	\$188,388	\$914,579	\$0.79
Total Membranes:		2300				Average



Cost Analysis





Norman Savings

36"-84 Membranes/support						
Well #	Asconc (ppb)	Replacements/yr	Membrane \$/yr	Elec \$/yr from ground + to holding tanks	Consumer Total Cost/yr	\$/1000 gallons treated
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Total Membranes:		3000				Average

Consumer Total Cost/yr includes:

- Membrane \$/yr found from dividing production costs per year by membranes produced in year plus a 15% mark-up
- Total electricity costs to pump water from well to holding tank

Save \$2.40/1000 gallons
of water treated

Save \$2.5 million per year!!!

At Home System

Average household water consumption (drinking water only): 7 gallons per day

Diameter of membrane: 1 inch (Size of faucet head)

ϵ	l_m (μm)	W_{pump} (kW)	Energy \$ of pump/yr	$t_{\text{saturation}}$ (day)	TCI	Membrane cost	Total product cost/year	Unit Price	Sales	Revenue
0.4	100	332	17	41	\$198,297	2.04	\$711,139	2.15	\$746,696	\$35,557
0.5	100	170	9	41	\$198,297	1.99	\$692,685	2.09	\$727,319	\$34,634
0.6	100	99	5	41	\$198,297	1.94	\$674,426	2.04	\$708,148	\$33,721

Treat 1 household per year
\$23.18

Average # of households
38,834

Cost to treat for all houses
\$900,077

Water treated for all households (gal/yr)
99,220,870

\$/1000 gallons of treated water
\$9.07

The background of the slide is a collage of US one hundred dollar bills, oriented in various directions and overlapping each other. The bills are semi-transparent, allowing the text to be clearly visible.

Conclusions

- 36 inch steel support of membranes proves most economically feasible
- Saves City of Norman \$2.5 million per year
- At home system is not economical
- Norman now in compliance with WHO regulations

Recommendations

- **Increase Product Markup**
 - Norman only saves \$500,000/yr
- **Consider On-Site Regeneration Services**
- **Expand to Other Cities with Arsenic Problems**
- **Research Membrane Mechanics**
 - Increase Porosity
 - Increase Thickness
 - Study Mechanical Integrity

A photograph of a fountain with water spraying upwards, creating concentric ripples on the surface. The word "Questions?" is overlaid in the center in a bold, black, sans-serif font. The background is a clear blue sky.

Questions?